



WALLACE H. COULTER SCHOOL OF ENGINEERING
Technology Serving Humanity

MEMORANDUM

Subject: Progress Report

ULI: FY13 Q3 Progress Report (4/1/2013–6/30/2013)

This document provides a progress report on the project “Advanced Digital Signal Processing” covering the period of 4/1/2013–6/30/2013.

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Revolutionary Research . . . Relevant Results

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Advanced Digital Signal Processing for Hybrid Lidar

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Presented to:

Annual ULI program review attendees

June 6, 2013

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Outline



- Background and Objectives
- Approach and Challenges
- Light Propagation in Water
- Progress
 - New ranging technique
 - New backscatter reduction technique
- Summary



Background and Objectives

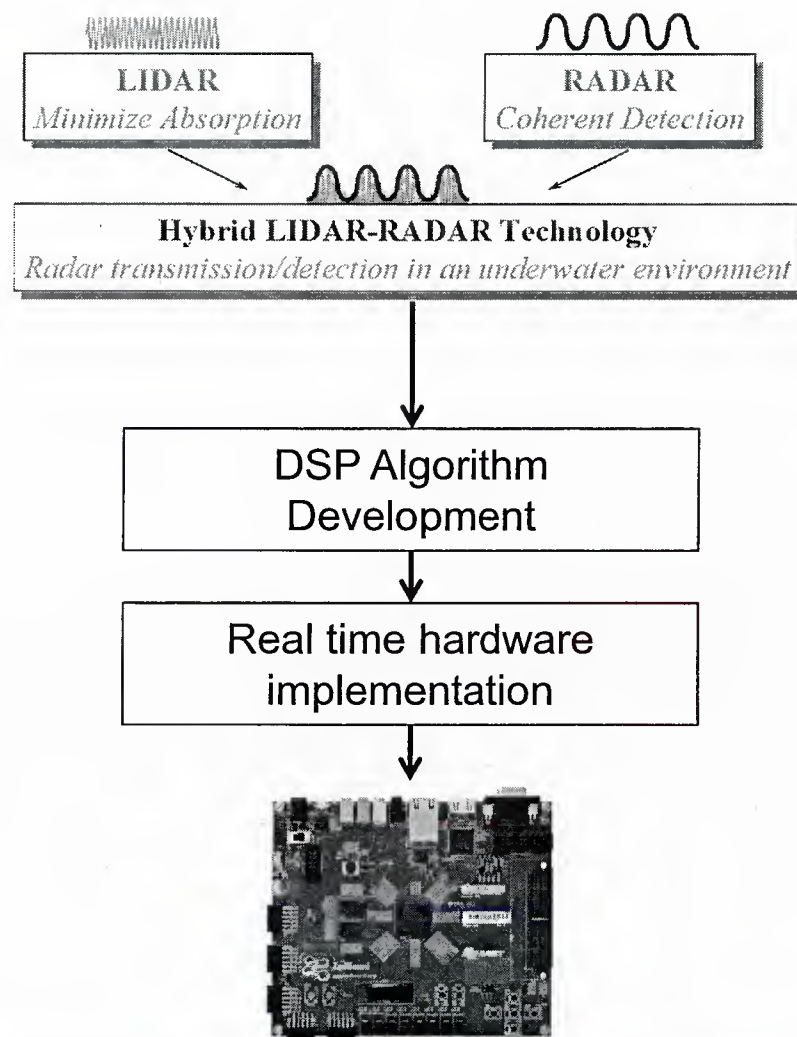


Background: The Navy uses hybrid lidar-radar for underwater detection, ranging, communications, and imaging.

- Modulate intensity of lidar laser signal with radar (RF) waveforms
- Recover radar waveform from received lidar optical signal
- Apply coherent detection and other radar techniques to process received signal.

Objectives: Enhance hybrid lidar-radar performance:

- Develop and evaluate various digital signal processing (DSP) algorithms that will enhance hybrid lidar-radar performance in a variety of underwater environments.
- Implement algorithms via DSP hardware:
 - dynamically reconfigured via software (accomplish multiple missions with a single sensor)
 - real-time processing
 - reduced loss/temperature sensitivity





Approach and Challenges



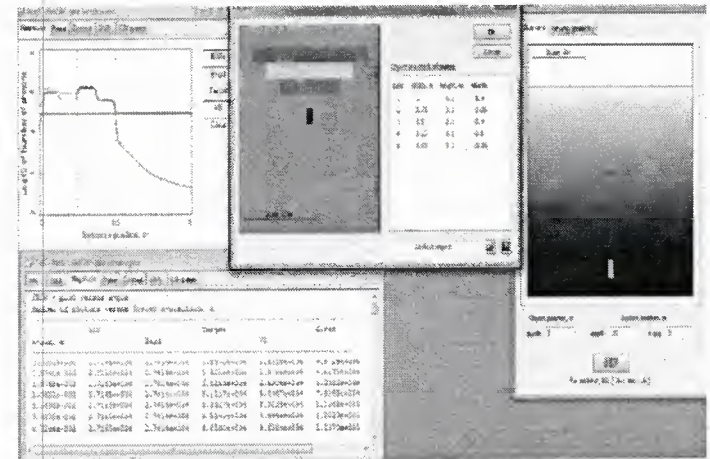
Approach:

- Leverage algorithms that are widely used in radar and wireless communications
 - Spatial filtering
 - Frequency domain reflectometry
 - Blind signal separation

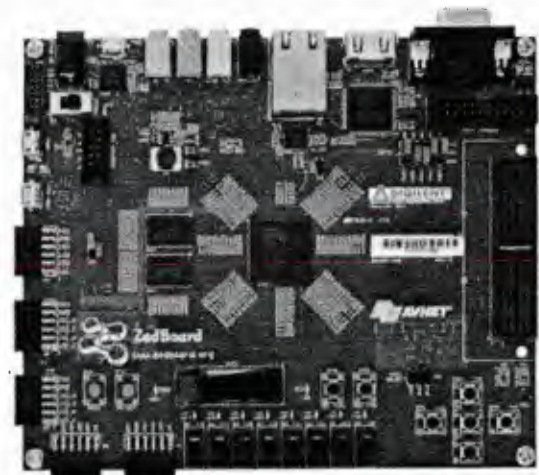
Challenges:

- The underwater propagation channel is very different than the above-water environment
 - Use an underwater (UW) optical propagation model, Rangefinder, to generate simulated data to test DSP algorithms
- Many COTS DSP hardware platforms (e.g. software defined radios) are suitable for above-water radar communications but lack performance for UW light detection and ranging
 - Utilize FPGAs tailored for application

Rangefinder



Xilinx Zynq FPGA Platform



Performance Goals

Simultaneously achieve:

high range resolution, range accuracy, range precision, and unambiguous range

1. Range resolution

- Indicates ability to resolve closely spaced targets

2. Range accuracy

- Indicates how close measurements are to the true range value

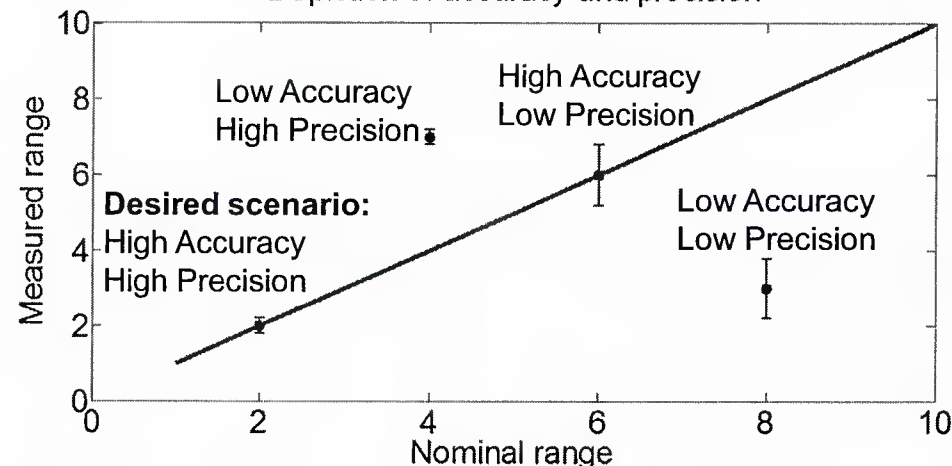
3. Range precision

- Indicates how closely multiple measurements are clustered together

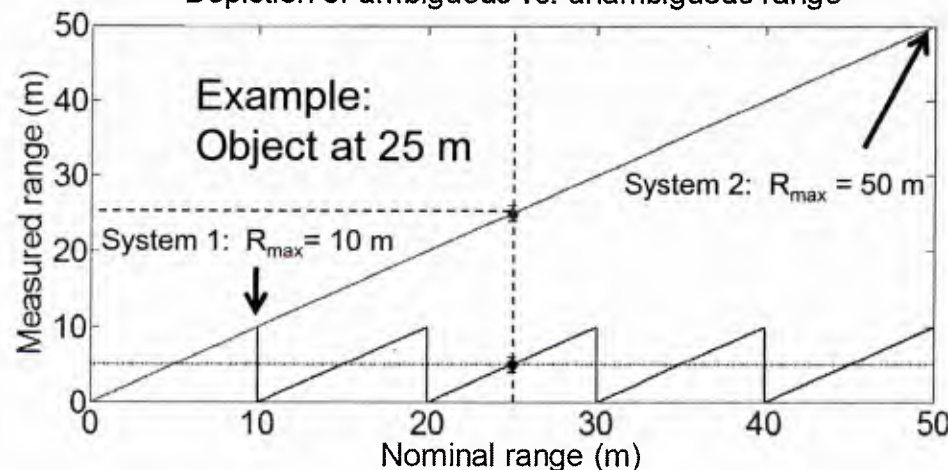
4. Unambiguous range

- R_{\max} indicates maximum distance at which true range is determined with no ambiguity

Depiction of accuracy and precision



Depiction of ambiguous vs. unambiguous range





Progress and Activity



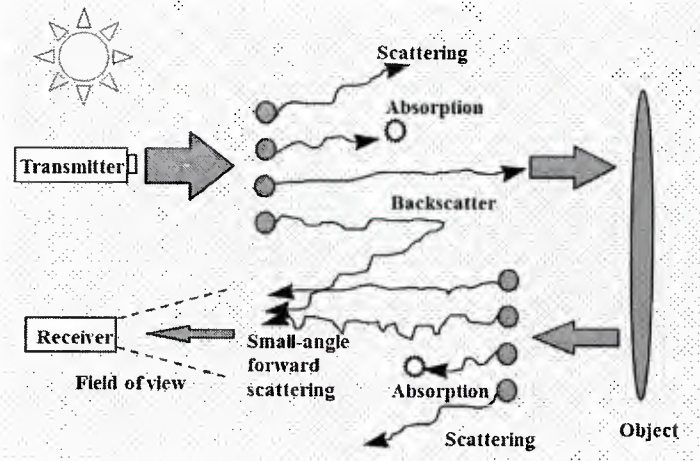
- Project start: June 2011
- Year 1
 - Participated in ONR NREIP program at NAVAIR
 - Assisted with water tank experiments
 - Characterized software defined radios
 - Identified, validated new lidar backscatter reduction technique: spatial filter
- Year 2
 - Participated in ONR NREIP program at NAVAIR
 - Spatial filter experiments
 - Identified new ranging technique: frequency-domain reflectometry
 - Identified new backscatter reduction technique: blind signal separation
- Summer 2013 (planned)
 - Participate in ONR NREIP program at NAVAIR
 - Thorough evaluation of new techniques
 - Validate new techniques with laboratory experiments
- Publications
 - "Underwater Laser Rangefinder," Proceedings of SPIE 2012, Ocean Sensing and Monitoring IV, Volume 8372
 - "Techniques to enhance the performance of hybrid lidar-radar ranging systems," Proceedings of MTS/IEEE Oceans 2012
 - "Technique to Extend Unambiguous Range of Hybrid Lidar-Radar Systems," Proceedings of MTS/IEEE Oceans 2013 (submitted)



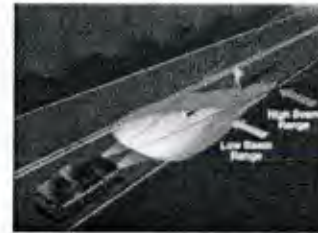
Light propagation in water



- Absorption decreases the total signal level at the receiver
- Scattering degrades image contrast, resolution, and reduces range accuracy



Absorption vs. Scatter-Limited Performance



Absorption-limited detection – more light, more range



Scatter-limited detection – more light, more 'clutter'

- Although absorption and scattering are two separate phenomena, their effects on water conditions are often combined together into a single parameter, the attenuation coefficient c (units: m^{-1})
- Beam attenuation in water follows an exponential decay law, where cz is the number of attenuation lengths (a.l.) :

$$P(c, z) = P_0 \exp(-cz)$$

After traveling one attenuation length, the optical beam is attenuated by a factor of $1 - \frac{1}{e} \approx 63.21\%$

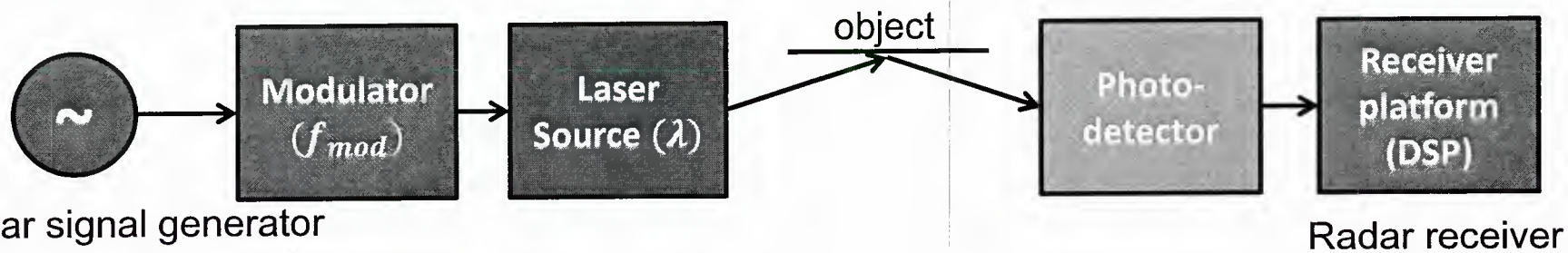
- We are focusing on enhancing performance in scatter-limited scenarios



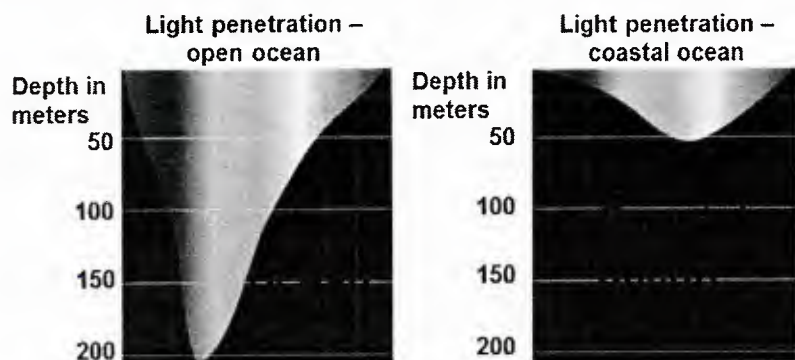
Three ways to improve performance in backscatter-limited scenarios



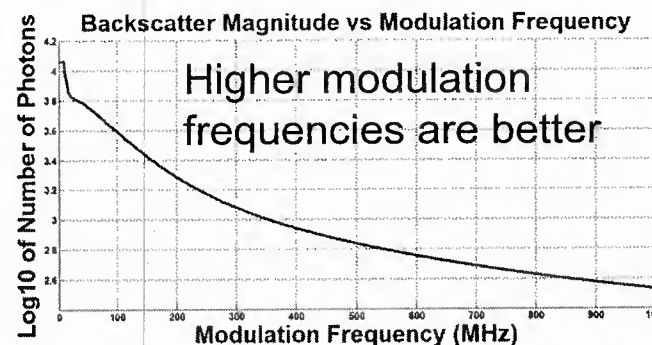
Simplified lidar-radar system



1. Wavelength Selection (λ)

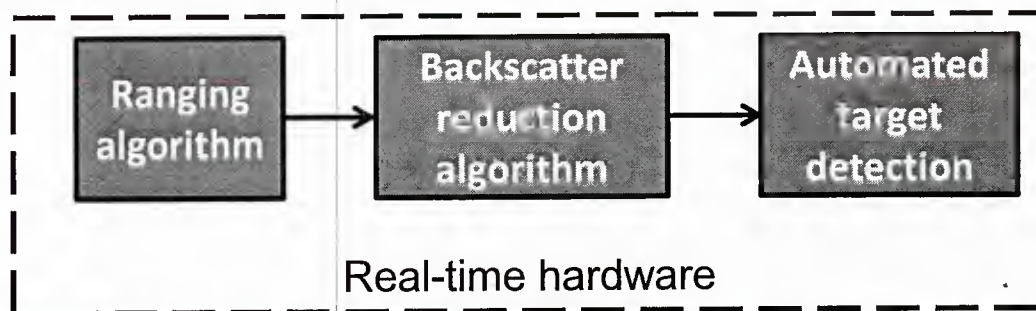


2. Modulation Frequency Selection (f_{mod})



3. Digital Signal Processing (DSP)

Our focus is to apply DSP algorithms to the receiver platform in order to **improve performance by processing the received signal.**

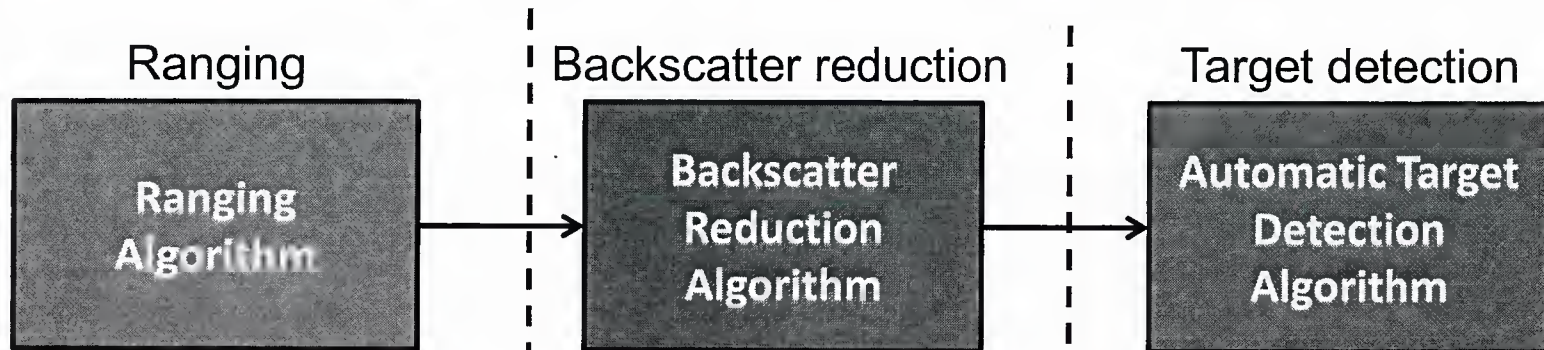




Technical Results Overview



Goal: automatically detect a target and calculate range
without any *a priori* knowledge



Approaches:

1. Single/Dual Tone

Spatial Filter

Phase to Range

2. Frequency Domain
Reflectometry

Blind Signal
Separation

Peak Detection

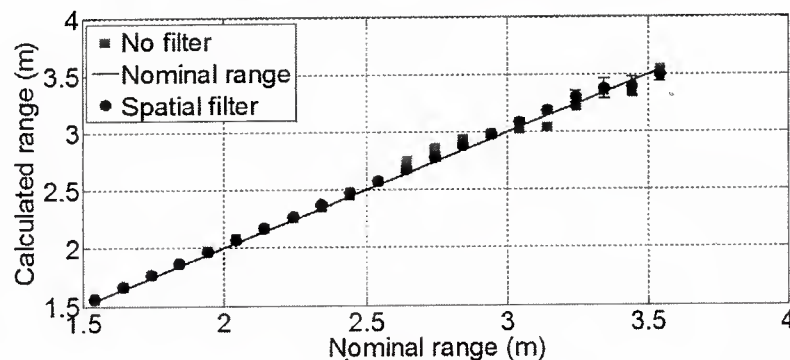


Approach #1: Spatial Filter Results

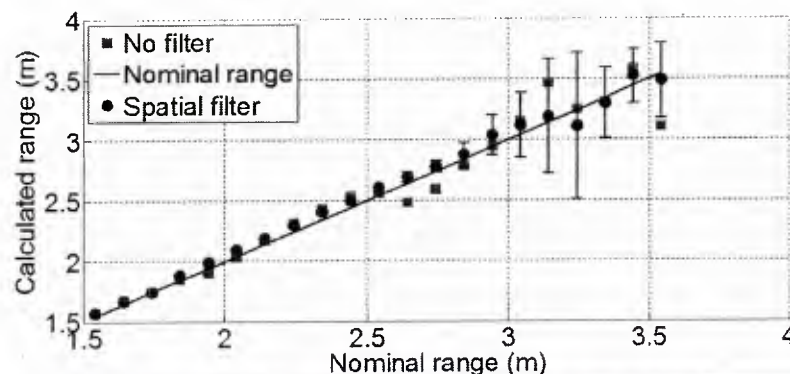


Results from 2012 Experiments, $c = 2.5 \text{ m}^{-1}$

Single-tone ranging with $f_m = 140 \text{ MHz}$

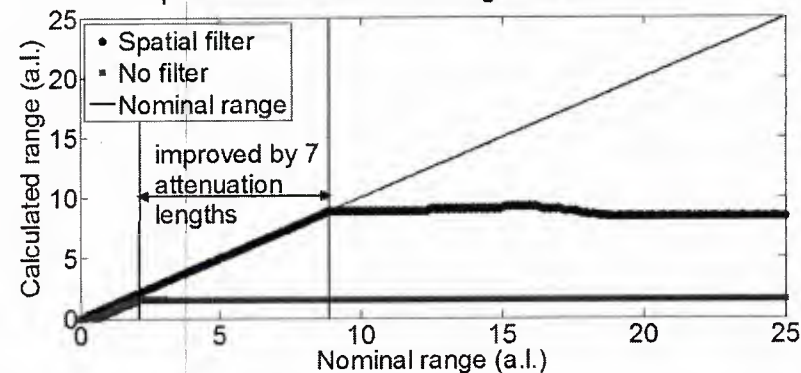


Dual-tone ranging with $f_1 = 140 \text{ MHz}$, $f_2 = 180 \text{ MHz}$

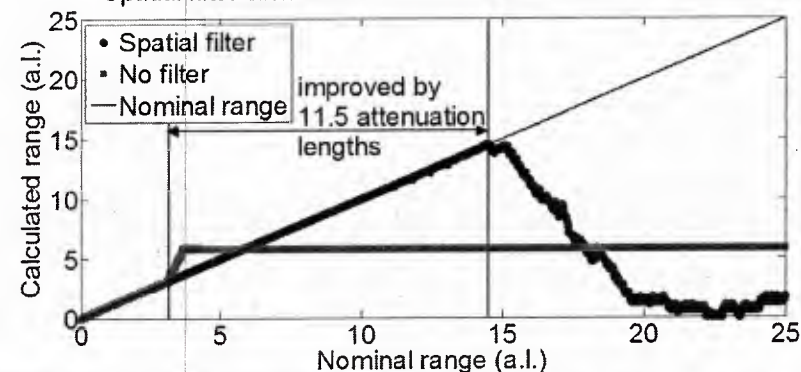


Simulation of Theoretical Performance

Spatial filter simulation for single-tone at 140 MHz



Spatial filter simulation for dual-tone at 140 and 180 MHz



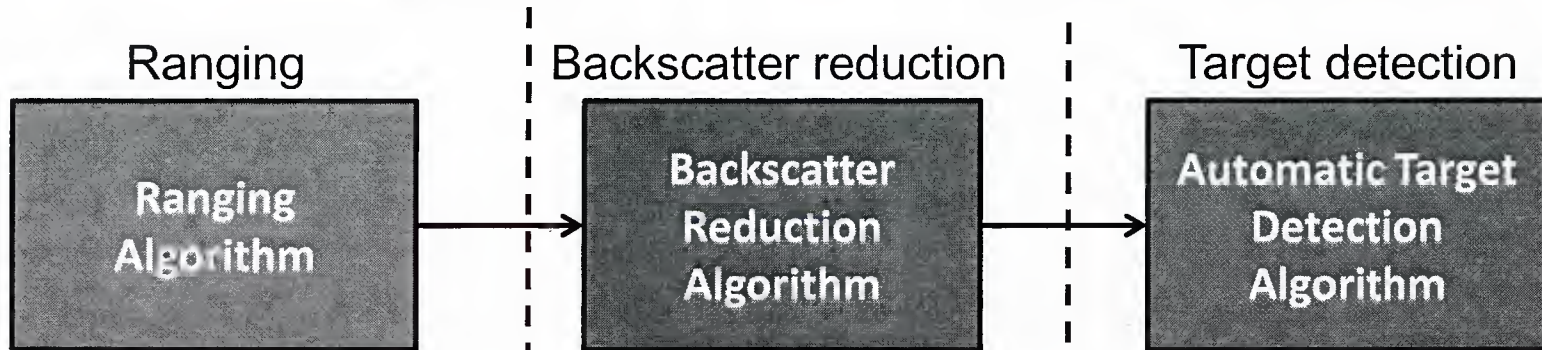
Range Algorithm	Unambiguous range	Range precision	Range Improvement with Spatial Filtering
Single-tone 140 MHz	0.80 m	2.65 cm	7 a.l.
Dual-tone 140, 180 MHz	2.81 m	12.40 cm	11.5 a.l.



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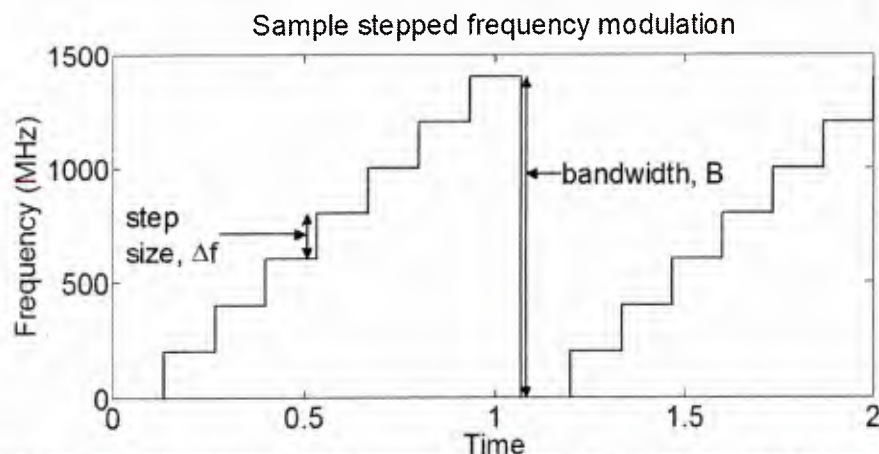
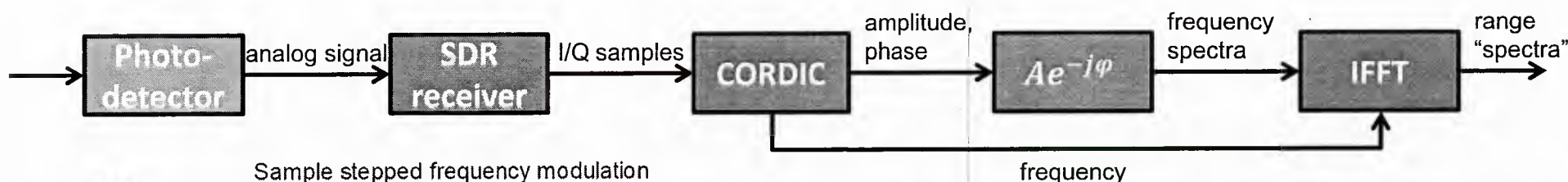
Peak Detection



Approach #2 Ranging Algorithm: Frequency-Domain Reflectometry (FDR)



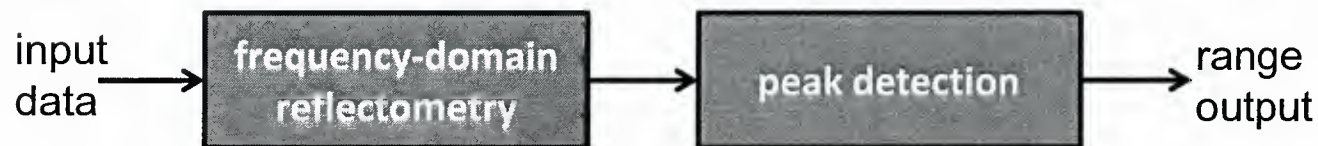
- FDR is a stepped frequency technique developed to detect faults in RF and fiber optic cables
- Small step size can lead to large unambiguous range performance
- Requires a large bandwidth to achieve comparable precision to CW methods



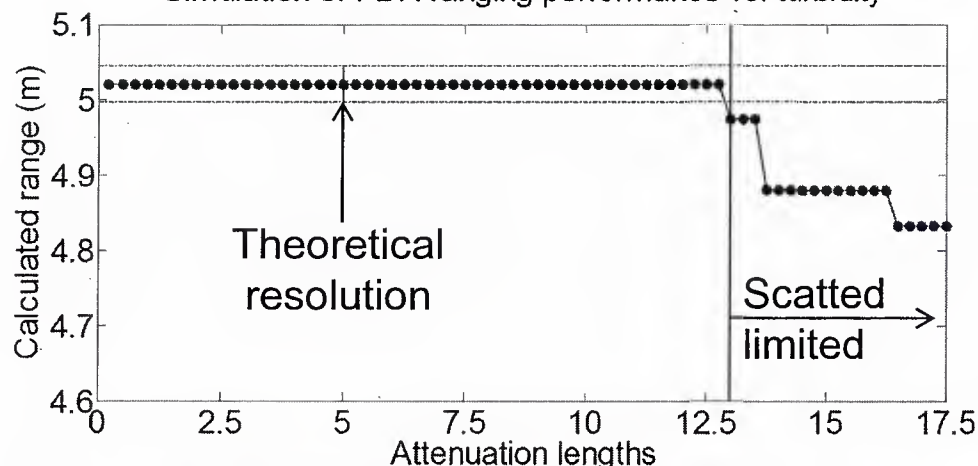
Parameter	Equation
Unambiguous range	$R_{max} = \frac{v}{2\Delta f}$
Range precision	$\delta R = \frac{v}{4B}$



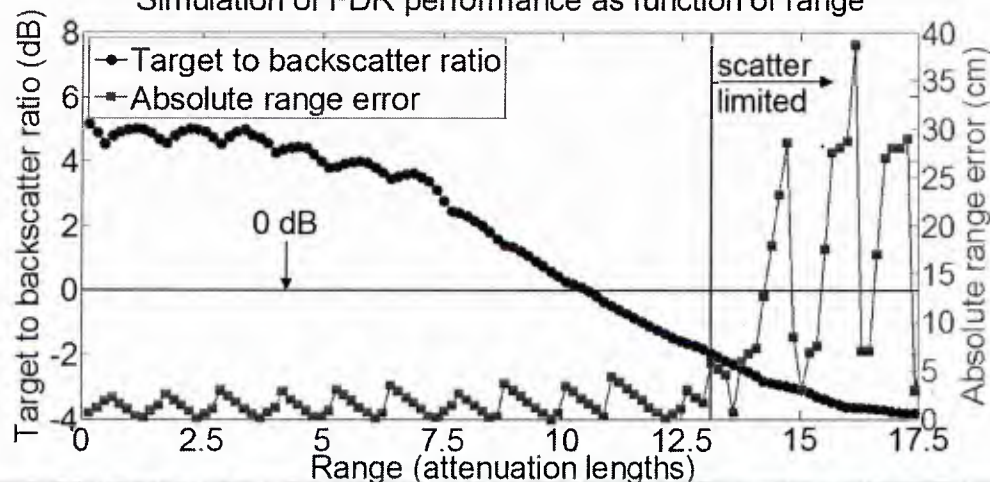
Approach #2: FDR Simulated Results with Automated Target Detection



Simulation of FDR ranging performance vs. turbidity



Simulation of FDR performance as function of range



Simulation: Fixed target range, varying turbidity.

- BW = 1.2 GHz;
- $\Delta f = 1.17$ MHz;
- $\delta R = 4.69$ cm;
- $R_{max} = 48.0$ m
- No backscatter reduction processing

Results: automated target detection works to 13 a.l. corresponding to target-to-backscatter ratios of -2 dB

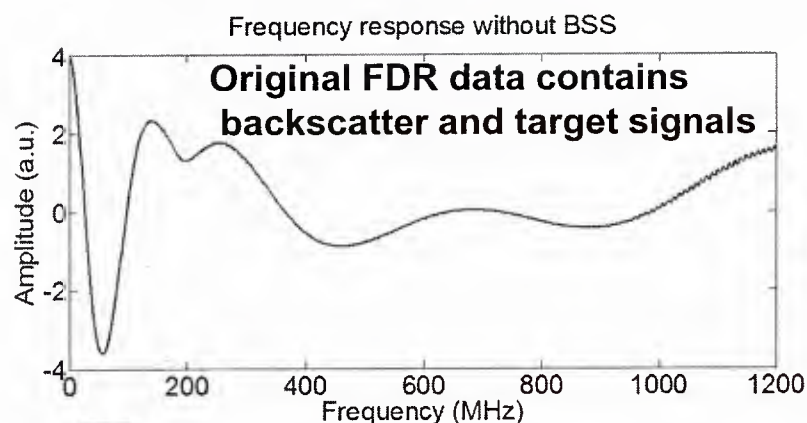
Next step: apply blind signal separation to reduce backscatter



Approach #2: Blind Signal Separation for Backscatter Reduction

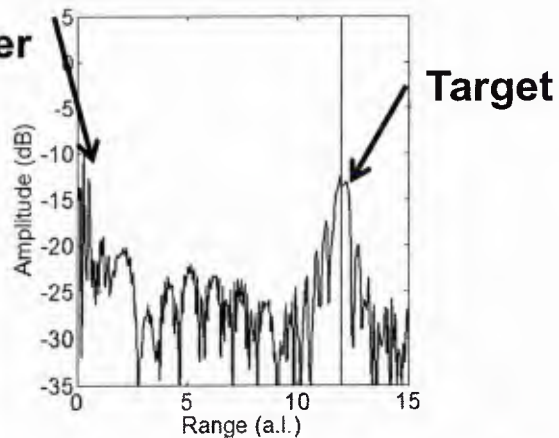
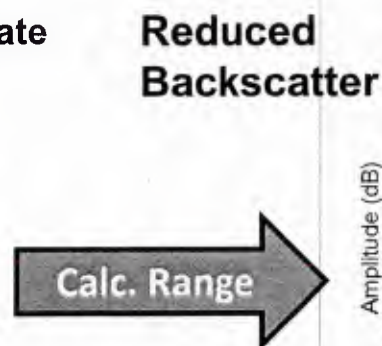
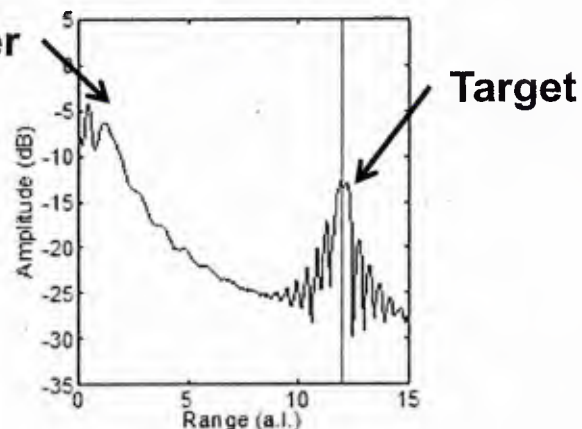
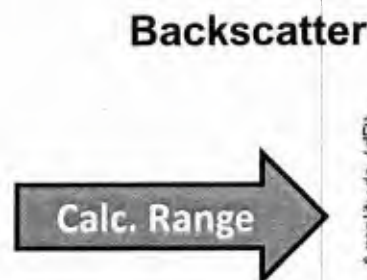
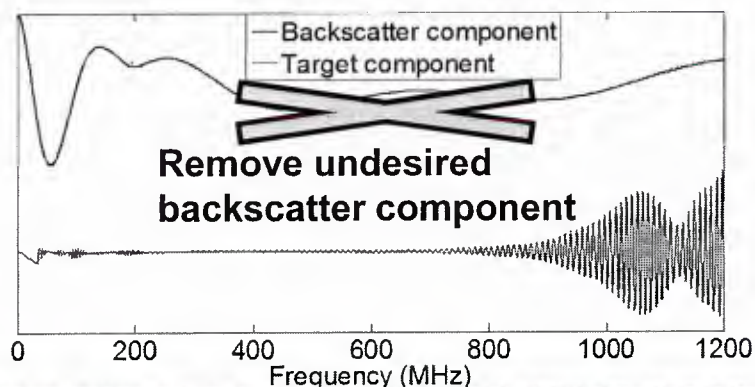


- Photons reflected from objects and backscatter in the scene are recorded as a single "mixed" lidar return
- Applying blind signal separation (BSS), the target and scatter components of the return can be separated



BSS separates the signal into separate backscatter and target signals

Frequency response of BSS components





Blind Signal Separation (BSS) Math Overview



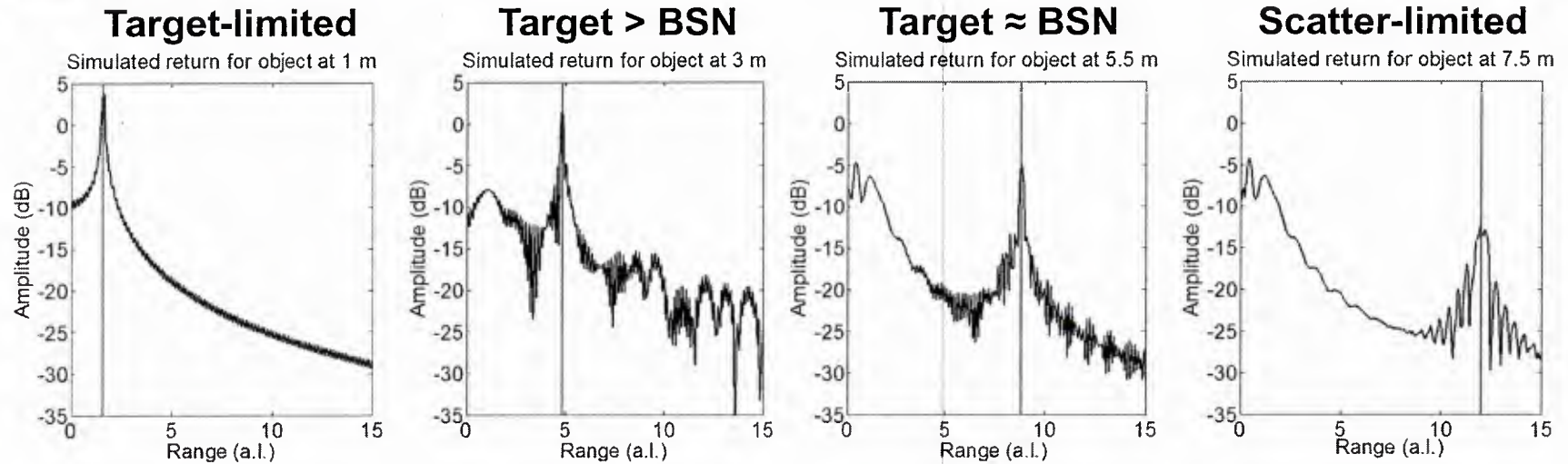
- Objective: Separate observations of several signals into the independent signal components based on their statistics
- Model: $X = AS$
 X : observation matrix, A : "mixing" matrix, S : source matrix
- Methodology: Select a statistical property. Adaptively learn a weight matrix $W \approx A^{-1}$ based on X . W should maximize separation based on the desired statistical property. At convergence, source components are estimated as $\hat{S} = WX \approx A^{-1}X$
- Challenges:
 - Choice of statistical property
 - Choice of convergence criteria
 - Estimation of number of sources
 - Choice of number of observations
 - Computational complexity



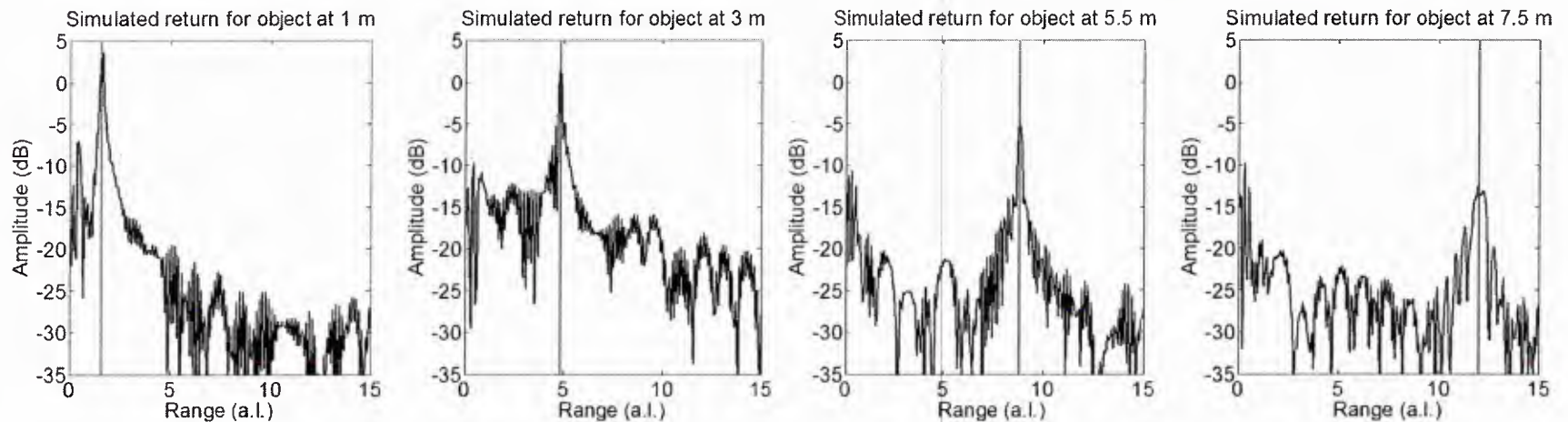
Approach #2: FDR Simulated Results with and without Backscatter (BSN) Reduction



no backscatter reduction



blind signal separation



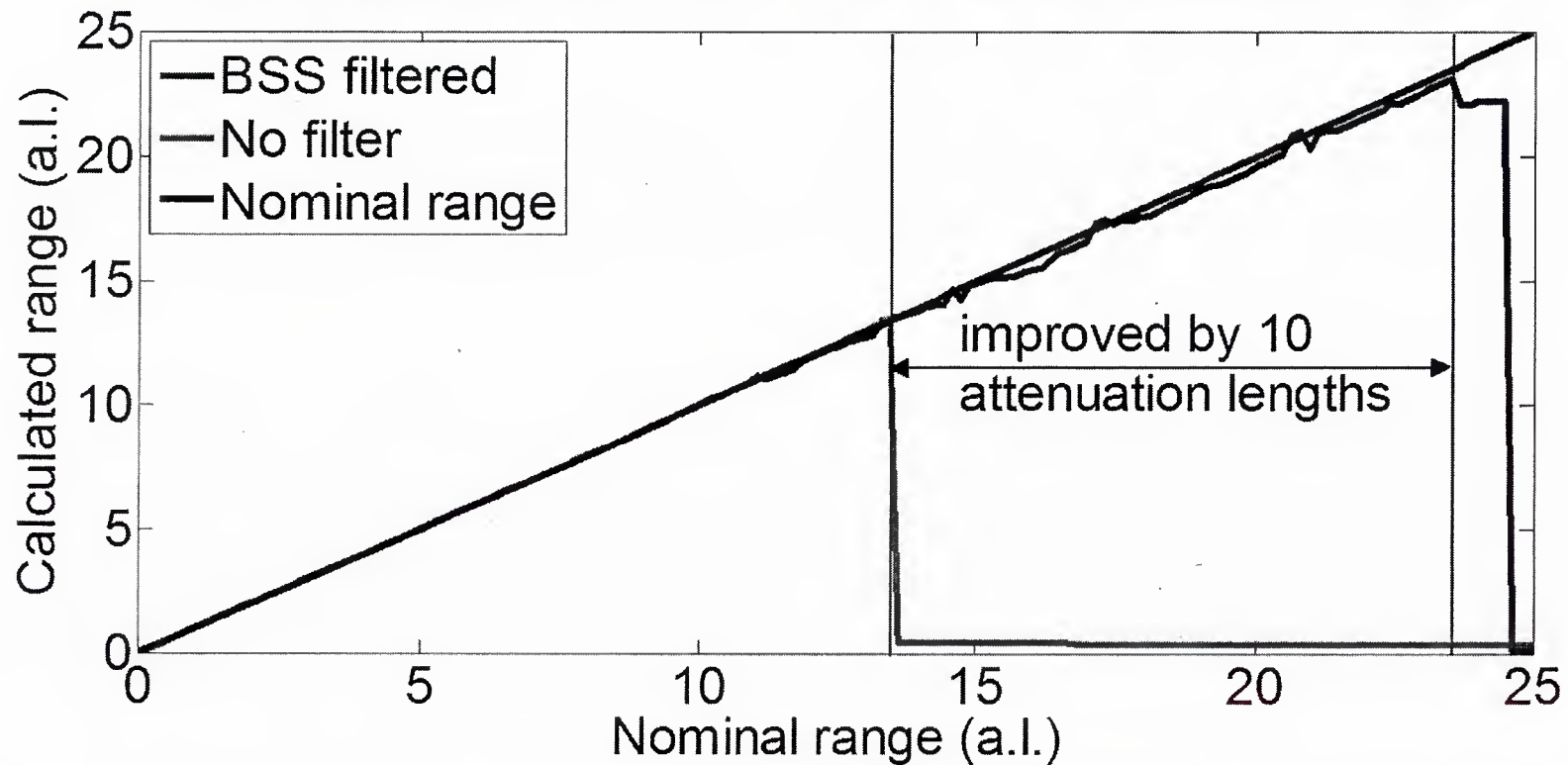
Green lines indicate actual target position
Range bin size: 9.38 cm; Turbidity: $c = 1.6 \text{ m}^{-1}$



Approach #2: FDR with BSS and Automated Signal Detection



BSS simulation for FDR w 1.2 GHz BW and 1024 tones



$$c = 1.6 \text{ m}^{-1}; \text{BW} = 1.2 \text{ GHz}; \Delta f = 1.17 \text{ MHz}$$

$$\delta R = 4.69 \text{ cm}; R_{\max} = 48.0 \text{ m}$$



Real-Time Implementation



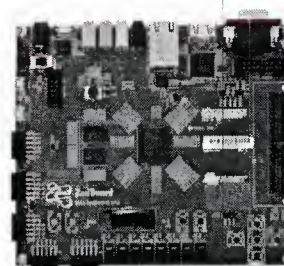
- Several basic building blocks have been implemented on real-time DSP hardware:
- Baseband demodulation
 - Decomposes RF signal into two orthogonal vectors
- CORDIC (COordinate Rotation DIgital Computer)
 - Given two vectors, finds the magnitude and phase angle of the resultant vector
 - The phase angle can be used to calculate range
- Instantaneous frequency demodulator
 - Calculates the frequency of the input signal

Example: demodulation of sinusoidal frequency modulated signal

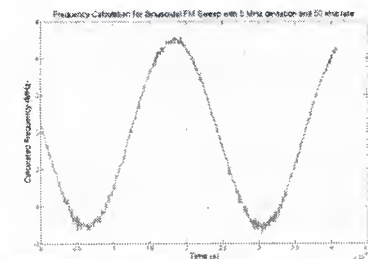
1. System design



2. Implementation



3. Calculation





Technique Comparison



Approach 1

Single- and Dual-Tone Ranging

- + short dwell time
- + very high precision
- single range result
- tradeoff between f_{mod} and R_{max}

Spatial Filter

- + computationally simple
- + single parameter
- logistically complicated
- implementation dependent on f_{mod}

Approach 2

Frequency-Domain Reflectometry

- + large unambiguous range
- + “range spectra”
- large bandwidth
- long dwell time

Blind Signal Separation

- + logistically simple
- + implementation independent of f_{mod}
- computationally complicated
- many parameters



Summary



- Significant progress has been made in developing a digital signal processing approach to enable hybrid lidar-radar ranging systems to perform automatic target detection:
 - Ranging: frequency-domain reflectometry technique provides large unambiguous range
 - Backscatter reduction: blind signal separation technique is able to separate the target and scatter returns
 - Target detection: simple peak detection algorithm is able to automatically detect target position
- Planned work
 - Experiments planned for summer 2013 to test performance of new technique as a function of range and turbidity
 - Continue to perform experiments with spatial filter method
 - MTS/IEEE Oceans Conference presentation in Fall 2013
 - Explore more sophisticated target detection algorithms that combine FDR and signal-tone approaches to improve precision
 - Develop real-time versions of each technique



Background Slides



Frequency-Domain Reflectometry (FDR) Overview



1. Transmit stepped frequency sweep with N tones
2. For each frequency f_i , record magnitude A_i and phase φ_i
3. Construct complex vector $S_i = A_i \exp(j\varphi_i)$
4. Calculate inverse Fourier transform of S_i :
$$s(t) = \frac{1}{2\pi} \int S(f) \exp(2\pi f t) df$$
5. Peaks appearing in the time-domain can be converted to range by multiplying by the speed of light



Frequency-Domain Reflectometry (FDR) Range Equation Derivation



- FDR range equations are based on applying Nyquist sampling theory in the frequency-domain
- Unambiguous range:
 - Frequency sample spacing: Δf
 - Maximum sampling time: $t_{max} = \frac{1}{\Delta f}$
 - Convert to range: $R_{max} = \frac{v}{2} t_{max} = \frac{v}{2\Delta f}$
- Range precision:
 - Time bin size: $\delta t = \frac{1}{2N} t_{max} = \frac{1}{2N\Delta f} = \frac{1}{2B}$
 - The factor of one-half is needed because the maximum error is half the size of a bin
 - Convert to range: $\delta R = \frac{v}{2} \delta t = \frac{v}{4B}$



Blind Signal Separation (BSS) Math Overview



- Objective: Separate observations of several signals into the independent signal components based on their statistics
- Model: $X = AS$
 X : observation matrix, A : "mixing" matrix, S : source matrix
- To separate components based on variance:
 1. Calculate sample covariance matrix $C = X^T X$
 2. Apply singular value decomposition:
$$X = USV^T$$

 U : projection of X onto eigenvectors of C , S : diagonal matrix of eigenvalues of C , V : eigenvectors of C
 3. Remove undesired components by "zeroing-out" columns of U and corresponding rows of S to obtain U_0 and S_0
 4. Calculated filtered observations as $X_{filt} = U_0 S_0 V^T$